

AMENDMENTS TO THE SPECIFICATION**IN THE SPECIFICATION:****Page 7**

Please amend the paragraph beginning at line 4, through line 12, as indicated below:

The calculation of the amount of discharged particulates includes: downloading data on an amount of intake air and data on an amount of injected fuel: calculating an excess air ratio λ in the given time period Δt on the basis of the amount of intake air and the amount of injected fuel; calculating an excess air ratio frequency $\gamma \Delta t$ in, in which the excess air ratio λ is the predetermined value or less in the given time period Δt , on the basis of the excess air ratio λ ; and calculating the amount of discharged particulates $Ma \Delta t \{-f(\gamma \Delta t)\}$ $Me \Delta t \{=f(\lambda \Delta t)\}$.
The foregoing procedures are sequentially executed.

Please amend the paragraph beginning at line 17, through line 30 as indicated below:

Further, the calculation of the amount of burnt particulates includes: downloading a catalyst temperature gt ; calculating a filter gas temperature frequency $\beta \Delta t$ in a given time period Δt on the basis of the catalyst temperature gt ; correcting the filter temperature frequency $\beta \Delta t$ using a correction factor K which depends upon an index $NO_x/Soot$ representing that components of exhaust gas are suitable for burning particulates; calculating a burning velocity coefficient $\alpha \Delta t \{=f(\beta \Delta t)\}$ for the given time period Δt ; and calculating an amount $Mb \Delta t$

$\{\alpha \Delta t \times PM_{i-1}\}$ of burnt particulates on the basis of an amount ~~PM_{i-1}~~ Ma_{i-1} of previously accumulated particulates and the burning velocity coefficient $\alpha \Delta t$, the foregoing procedures being conducted in the named order.

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Please amend the paragraph beginning at line 21, through line 28 as indicated below:

During the forced regeneration control, the following are calculated: the amount Me of discharged particulates in step s1; the amount Mb of burnt particulates in step s2; and the amount Ma of accumulated particulates in step s3. When the amount Ma of accumulated particulates is equal to a predetermined threshold ~~$Ma \propto$~~ Ma_{ϵ} in step s4, the control process is advanced to step s5, where the forced regeneration control will be performed in order to forcibly regenerate the filter 22 (e.g. post-injection control will be carried out for a predetermined time period).

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Please amend the paragraphs beginning at line 21, through page 13, line 2 as indicated below:

~~The amount Ma~~ The amount of Ma_i of currently accumulated particulates is added to the ~~amount Ma~~ an amount Ma_{i-1} of particulates previously accumulated during a predetermined time period mt , so that a total amount $Maptm$ of particulate is derived.

In step s4, it is checked whether or not the total amount $Maptm$ is above the predetermined threshold ~~$Ma \propto$~~ Ma_{ϵ} . The calculations in steps s1 to s4 are repeated until the

amount M_{apm} is above the predetermined threshold $M_{ae} \underline{M_{a\epsilon}}$. The threshold $M_{ae} \underline{M_{a\epsilon}}$ is determined in order to prevent the filter 22 from being overheated and damaged when particulates thereon are continuously burnt.

When $M_{apm} > M_{ae} \underline{M_{a\epsilon}}$, post-fuel injection is conducted for a predetermined time period in step s5 in order to forcibly heat and regenerate the filter 22. Specifically, as shown in Fig. 7, not only an amount IN_{jn} of fuel injected (for an injection period B_m) in the main injection J1 but also a fuel injection timing t_1 are calculated in accordance with a current state of the engine 2. Further, a post injection amount IN_{jp} of fuel to be post-injected (for an injection period B_s) is set to a fixed value at a fuel injection timing t_2 after the main fuel injection.

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Please amend the paragraph beginning at line 13, through line 14 as indicated below:

Referring to Fig. 4(b), the excess air ratio frequency γ_i at the end of calculation in the time period Δt is assumed to be $\gamma_{\Delta t} \underline{\lambda \Delta t}$.

Please amend the paragraphs beginning at line 27, through line 35 as indicated below:

A section a2-2' calculates an amount $M_{a\Delta t} \underline{M_{e\Delta t}}$ of particulates discharged during the time period Δt , using the formula (i).

$$\underline{M_{a\Delta t} M_{e\Delta t}} = f(\gamma_{\Delta t}) f(\underline{\lambda \Delta t}) \quad \dots (i)$$

Further, the amount M_e of discharged particulates may be derived by multiplying the excess air ratio frequency $\gamma_{\Delta t} \underline{\lambda \Delta t}$ (in the time period Δt) by a predetermined coefficient C.

The coefficient C is experimentally determined. Still further, the amount Me may be derived using a map in which the amount Me of discharged particulates is depicted on the basis of the excess air ratio frequency $\gamma \Delta t$, in place of using the formula (i).

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Please amend the paragraph beginning at line 23, through line 25 as indicated below:

Alternatively, the amount $M_b \Delta t$ may be derived using a map showing the relationship between the ~~particulate burning velocity $\beta \Delta t$~~ particulate burning velocity coefficient $\alpha \Delta t$ and the amount M_b of burnt particulates.

Please amend the formula beginning at line 30 as indicated below:

$$PM_i = PM_{i-1} + (\cancel{Ma \Delta t} \underline{Me \Delta t} - M_b \Delta t) \times \Delta t \cdots \cdots (m)$$

Please amend the formula beginning at line 36 as indicated below:

$$PM_i = PM_{i-1} + (\cancel{Ma \Delta t} \underline{Me \Delta t} - \alpha \Delta t \times PM_{i-1}) \times \Delta t \cdots \cdots (n)$$

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Please amend the paragraph beginning at line 4, through line 6 as indicated below:

The amount ~~$Ma \Delta t$~~ $Me \Delta t$ of particulates discharged in the time period Δt is calculated in step s10, and the amount $M_b \Delta t$ of burnt particulates in the time period Δt is calculated in step s20.

Please amend the paragraph beginning at line 7, through line 13 as indicated below:

A routine shown in Fig. 9(b) is used for this purpose. In step s11, an intake air amount Q_a and a fuel injection amount Q_f are downloaded. In step s12, the excess air ratio λ in the time period Δt is calculated on the basis of the downloaded data. In step s13, the excess air ratio frequency γ is calculated by the excess air ratio frequency calculator a2-1' shown in Fig. 8. Finally, the amount $\cancel{M_a \Delta t} \underline{M_e \Delta t} \{= f(\gamma \Delta t)\}$ is calculated in step s14.

Please amend the paragraph beginning at line 23, through line 25 as indicated below:

Following the calculations of $\cancel{M_a \Delta t} \underline{M_e \Delta t}$ and $M_b \Delta t$ in steps s10 and s20, the amount PM_i of currently accumulated particulates is calculated using PM_{i-1} , $\cancel{M_a \Delta t} \underline{M_e \Delta t}$ and $M_b \Delta t$ in step 30. Refer to Fig. 9(a).

Please amend the paragraph beginning at line 34, through page 18, line 2, as indicated below:

The amount PM_i of accumulated particulates can be accurately detected by calculating the amount $\cancel{M_a} \underline{M_e}$ of particulates discharged in the time period Δt and the amount M_b of particulates burnt in the time period Δt . Therefore, forced regeneration intervals can be properly set up and lengthened, which is effective in preventing the reduction of fuel efficiency.

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Please amend the paragraph beginning at line 3, through line 6 as indicated below:

Further, the burnt particulate amount calculating unit A2' may derive the filter temperature frequency $\beta_{\underline{t_c}}$, where a filter temperature $\geq 250^{\circ}\text{C}$ or higher for the time period Δt , or may derive an average of the filter temperature frequency $\beta_{\underline{t_c}}$ in the time period Δt .